



# Efficient electrosynthesis of *n*-propanol from carbon monoxide using a Ag–Ru–Cu catalyst

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**The high-energy-density C<sub>3</sub> fuel *n*-propanol is desired from CO<sub>2</sub>/CO electroreduction, as evidenced by propanol's high market price per tonne (approximately US\$ 1,400–1,600). However, CO electroreduction to *n*-propanol has shown low selectivity, limited production rates and poor stability. Here we report catalysts, identified using computational screening, that simultaneously facilitate multiple carbon–carbon coupling, stabilize C<sub>2</sub> intermediates and promote CO adsorption, all leading to improved *n*-propanol electrosynthesis. Experimentally we construct the predicted optimal electrocatalyst based on silver–ruthenium co-doped copper. We achieve, at 300 mA cm<sup>-2</sup>, a high *n*-propanol Faradaic efficiency of 36% ± 3%, a C<sub>2+</sub> Faradaic efficiency of 93% and single-pass CO conversion of 85%. The system exhibits 100 h stable *n*-propanol electrosynthesis. Technoeconomic analysis based on the performance of the pilot system projects profitability.**

The electrochemical reduction reaction of carbon dioxide (CO<sub>2</sub>RR) to valuable fuels and chemical feedstocks offers a promising route to store intermittent renewable electricity<sup>1–5</sup>. However, present-day CO<sub>2</sub>RR studies have been performed predominantly in alkaline/neutral electrolytes with a local pH > 7 at the catalyst surface during the reaction, leading to the loss of CO<sub>2</sub> through bicarbonate/carbonate formation and added cost for CO<sub>2</sub> regeneration<sup>6</sup>. The electrochemical reduction reaction of carbon monoxide (CORR) following the CO<sub>2</sub> reduction to CO, a two-step cascade process, overcomes this problem<sup>6–8</sup>. Owing to advances in solid oxide electrolysis cell technology, a CO feedstock can now be produced from CO<sub>2</sub> at low cost with an energy efficiency of 90% at ~200 mA cm<sup>-2</sup>, furthering applications of CORR<sup>9–11</sup>.

Among reported C<sub>1</sub>–C<sub>3</sub> products in CORR, the C<sub>3</sub> alcohol *n*-propanol is particularly desirable in light of its high energy density and high octane number. It is suitable as an engine fuel, as a solvent and as a feedstock for *n*-propyl acetate<sup>12,13</sup>. Today, *n*-propanol is mainly manufactured via the hydroformylation of ethylene with CO and H<sub>2</sub> to form propionaldehyde, followed by the hydrogenation of propionaldehyde under high pressure and temperature<sup>12</sup>. This complex manufacturing process increases cost and thus limits the overall size of the *n*-propanol market<sup>13</sup>; yet, in light of its higher energy density, *n*-propanol could take the place of ethanol as a transportation fuel additive for which the market would grow if *n*-propanol could be efficiently produced. Hence, it is attractive to explore whether *n*-propanol could be generated efficiently through electrolysis using renewable electricity<sup>13,14</sup>.

The present-day performance of *n*-propanol electrosynthesis—including selectivity, production rate and stability—remains low and far below the requirements of practical applications. Technoeconomic analysis (TEA) has shown that reaction rates must exceed at least 100 mA cm<sup>-2</sup> for profitable CORR systems<sup>7</sup>.

Experimentally, previous CORR/CO<sub>2</sub>RR systems with current densities above 100 mA cm<sup>-2</sup> have shown limited selectivity towards *n*-propanol, with a maximum Faradaic efficiency (FE) of 18% and little information on operando stability (Supplementary Table 1)<sup>6,15–20</sup>.

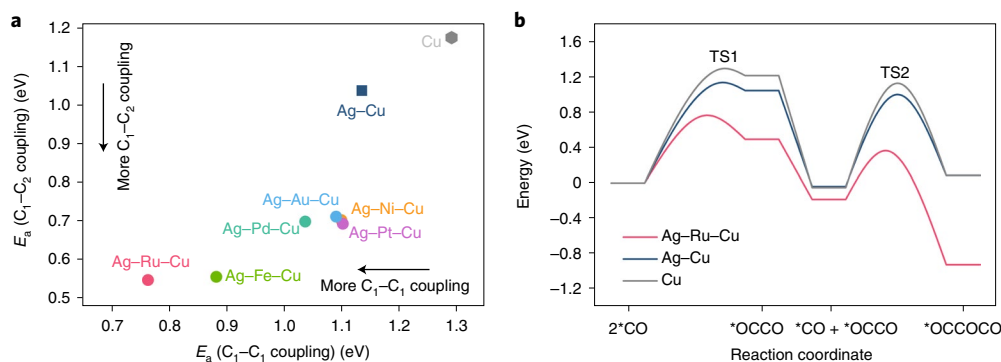
The generation of C<sub>3</sub> in CORR relies on C<sub>1</sub>–C<sub>1</sub> coupling and subsequent C<sub>1</sub>–C<sub>2</sub> coupling. The key step branching the pathways to C<sub>3</sub> and C<sub>2</sub> products is identified as coupling between C<sub>1</sub> and C<sub>2</sub> intermediates<sup>21,22</sup>. To ensure the production of C<sub>3</sub> at high production rates, C<sub>2</sub> intermediates must be formed and stabilized on the catalyst surface and thus be available to be coupled with adsorbed CO (ref. 16).

We took the view, therefore, that to promote C<sub>3</sub> selectivity at high production rates, a good catalyst would simultaneously facilitate both the C<sub>1</sub>–C<sub>1</sub> and the C<sub>1</sub>–C<sub>2</sub> coupling steps, stabilize C<sub>2</sub> intermediates and promote CO adsorption. In this Article, we present a catalyst design—silver–ruthenium co-doped copper (Ag–Ru–Cu) catalysts—with high selectivity, production rate and stability for *n*-propanol electrosynthesis. We report a *n*-propanol FE of 37% ± 3% at a production rate of 111 ± 9 mA cm<sup>-2</sup> in CORR, a more than two times improvement compared with the value reported at total current density above 100 mA cm<sup>-2</sup> (refs. 6,15–20) and 100 h stable *n*-propanol electrosynthesis at 300 mA cm<sup>-2</sup>. We further demonstrate scaling of *n*-propanol electrosynthesis on Ag–Ru–Cu catalysts to 15 cm<sup>2</sup>, which delivers an *n*-propanol FE of 36% ± 3% and a C<sub>2+</sub> FE of 93% with a high single-pass CO conversion of 85%.

## Theoretical calculations

We began by using density functional theory (DFT) calculations to screen catalyst systems considering their propensity to catalyse the C<sub>1</sub>–C<sub>1</sub> and C<sub>1</sub>–C<sub>2</sub> coupling. Ag-doped Cu (Ag–Cu) is an experimentally reported bimetallic catalyst that favours the selectivity to

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**Fig. 1 | DFT calculations on  $C_1-C_1$  and  $C_1-C_2$  coupling.** **a**, The calculated activation energy ( $E_a$ ) for  $C_1-C_1$  and  $C_1-C_2$  coupling on screened Ag-X-Cu, where X is Au, Pd, Pt, Ni, Fe and Ru. X is categorized into three different groups according to the CO adsorption energies with reference to Cu: (1) weak, Au; (2) intermediate, Pd, Pt and Ni; (3) strong, Fe and Ru. The  $E_a$  ( $C_1-C_1$  coupling) and  $E_a$  ( $C_1-C_2$  coupling) on Ag-Cu and Cu catalyst systems are also calculated for comparison. **b**, Reaction coordinate diagram for  $C_1-C_1$  and  $C_1-C_2$  coupling on Ag-Ru-Cu, Ag-Cu and Cu catalyst systems. TS1 and TS2 denote the transition state of  $C_1-C_1$  and  $C_1-C_2$  coupling, that is,  $^*CO-^*CO$  and  $^*CO-^*OCCO$ , respectively.

*n*-propanol compared with Cu (ref. 23). We therefore considered several Ag-X co-doped Cu (Ag-X-Cu, where X represents an additional metal) catalyst systems for computational screening (Fig. 1a, Supplementary Figs. 1–9 and Supplementary Tables 2 and 3). On the basis of previous studies<sup>16,17,21,23–28</sup>, we calculated the activation energies of the  $^*CO$  dimerization ( $^*CO + ^*CO \rightarrow ^*OCCO$ ) and the coupling between  $^*CO$  and  $^*OCCO$  intermediates ( $^*CO + ^*OCCO \rightarrow ^*OCCOCO$ ) on different Ag-X-Cu catalyst systems and then applied them as predictors for the activities of  $C_1-C_1$  and  $C_1-C_2$  coupling, respectively. Of the catalyst systems screened, Ag-Ru-Cu requires the lowest activation energies for both  $C_1-C_1$  and  $C_1-C_2$  coupling (Fig. 1a).

We further compared the adsorption energies of  $^*CO$  and  $^*OCCO$ , the key reaction intermediates associated with the  $C_1-C_1$  and  $C_1-C_2$  coupling<sup>16,17,23</sup>, on Ag-Ru-Cu versus those on Ag-Cu and Cu (Fig. 1b and Supplementary Fig. 10). Relative to Ag-Cu and Cu, the higher average  $^*CO$  adsorption energy on Ag-Ru-Cu indicates that CO molecules are more readily adsorbed on Ag-Ru-Cu. Specifically, the co-doping of Ag and Ru in Cu induces CO adsorption near the  $C_1-C_1$  and  $C_1-C_2$  coupling sites and thus results in higher  $^*CO$  coverage on the surface compared with Ag-Cu and Cu, which may promote multiple C-C coupling (Supplementary Tables 2 and 4). Additionally, the adsorption energy of the key  $C_2$  intermediate for  $C_1-C_2$  coupling on Ag-Ru-Cu is higher than that on Ag-Cu and Cu; this may reduce the desorption of  $C_2$  intermediates from the Ag-Ru-Cu surface and the subsequent formation of  $C_2$  products, thus increasing the residence of  $C_2$  intermediates necessary for  $C_3$  generation. These calculations, taken together, suggest that Ag-Ru-Cu has the potential to improve  $C_3$  selectivity at high production rates.

### Catalyst preparation and characterization

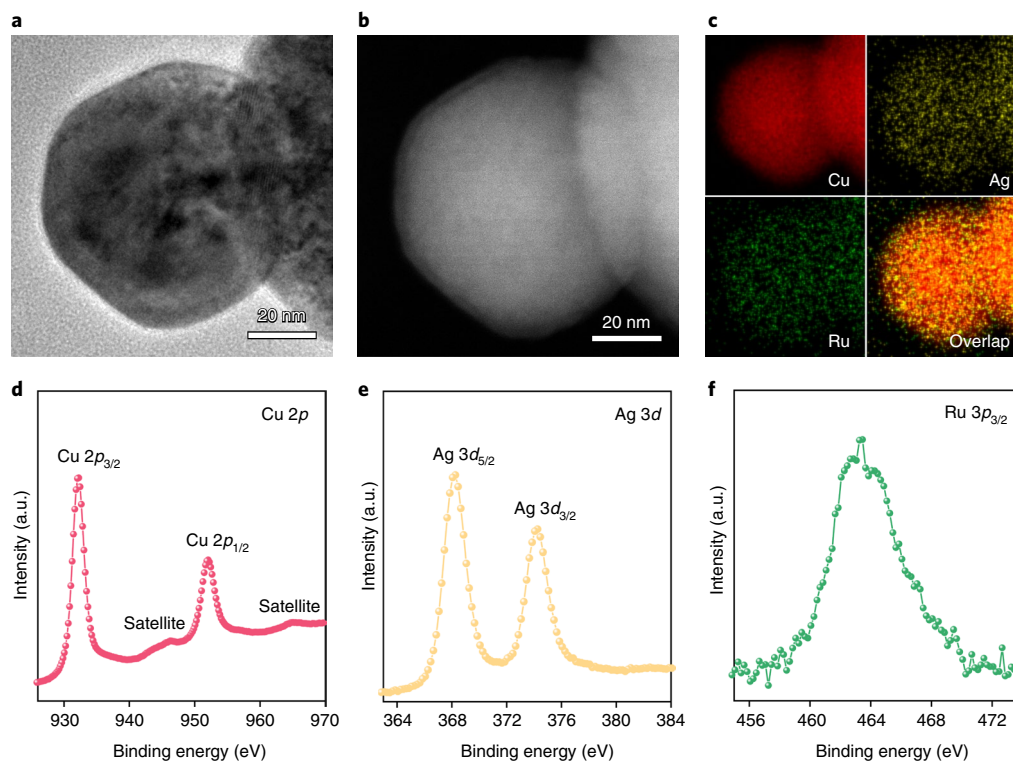
We sought to realize Ag-Ru-Cu catalysts experimentally. We first spray coated a layer of commercial Cu nanoparticles onto a gas-diffusion layer (Supplementary Fig. 11a). Then, we prepared the Ag-Ru-Cu catalyst (Fig. 2a,b and Supplementary Fig. 11b) via a two-step galvanic replacement between Cu and  $RuCl_3$  and then between Cu and  $AgNO_3$ —driven by the difference in the reduction potentials of Ru versus Cu and Ag versus Cu (refs. 29–31), respectively. We observed no appreciable difference in morphology for Ag-Ru-Cu versus the pristine Cu based on scanning electron microscopy (SEM; Supplementary Fig. 11). Energy-dispersive X-ray (EDX) spectroscopy elemental mapping reveals that Ag, Ru and Cu elements are evenly distributed in the Ag-Ru-Cu nanoparticles (Fig. 2c). In the powder X-ray diffraction (XRD) patterns of the Cu and

Ag-Ru-Cu electrodes, we observe peaks of  $Cu_2O$  ascribed to the partial oxidation of Cu nanoparticles in air during electrode preparation (Supplementary Fig. 12). High-resolution X-ray photoelectron spectroscopy (XPS) further confirms the existence of Cu, Ag and Ru in the nanoparticles (Fig. 2d–f and Supplementary Fig. 13). The atomic percentages of Ag and Ru in the electrode near the surface are approximately 4% and 1%, respectively, as determined using XPS.

### Investigation on electroreduction of CO

The CORR performance was evaluated in a membrane electrode assembly (MEA) electrolyser with both cathode and anode electrodes having a  $5\text{ cm}^2$  active geometric area ( $A = 5\text{ cm}^2$ ) (Supplementary Figs. 14 and 15). Figure 3a displays the FEs of  $C_{2+}$  products (ethylene, ethanol, acetate and *n*-propanol) on Ag-Ru-Cu and Cu electrodes during CORR in the current density range of  $200\text{--}600\text{ mA cm}^{-2}$ . Ag-Ru-Cu electrodes delivered higher selectivities to total  $C_{2+}$  products and to *n*-propanol, relative to Cu electrodes (Supplementary Table 5 and Supplementary Fig. 16), consistent with DFT predictions (Fig. 1). In the regime of  $300\text{--}600\text{ mA cm}^{-2}$ , the total FEs for  $C_{2+}$  products reach 90%, and the highest  $C_{2+}$  partial current density reaches  $540\text{ mA cm}^{-2}$  for the Ag-Ru-Cu electrodes (Fig. 3b). Specifically, under a current density of  $300\text{ mA cm}^{-2}$ , we achieve an *n*-propanol FE of  $37\% \pm 3\%$  on Ag-Ru-Cu electrodes—1.8 times higher than that on Cu electrodes—at a production rate of  $111 \pm 9\text{ mA cm}^{-2}$  associated with a full-cell potential of  $-2.75 \pm 0.01\text{ V}$ . This is a directly measured full-cell voltage; that is, it does not include any correction from ohmic losses.

To explore further the effect of co-doping Ag and Ru into Cu on CORR performance, we prepared Ag-Cu electrodes and measured their CORR performance for comparison. The Ag-Cu electrodes were prepared via the same galvanic-replacement approach, and the atomic percentage of Ag doping in Cu on the electrode surface was also approximately 4%, as determined by XPS (Supplementary Figs. 17–19). At the same current densities, the total FEs towards  $C_{2+}$  products on the Ag-Cu electrodes are higher than those on Cu electrodes but lower than those on Ag-Ru-Cu electrodes (Supplementary Table 5). This indicates that the Ag doping in Cu favours  $C_1-C_1$  coupling for  $C_{2+}$  products relative to Cu, and the co-doping of Ag and Ru further enhances the  $C_{2+}$  selectivity. The *n*-propanol FEs on different electrodes follow the sequence Ag-Ru-Cu > Ag-Cu > Cu (Fig. 3c), suggesting that co-doping of Ag and Ru in Cu also promotes the step of  $C_1-C_2$  coupling versus Ag-Cu and Cu, in agreement with calculations (Fig. 1). At  $500\text{ mA cm}^{-2}$ , the highest partial *n*-propanol current density on the Ag-Ru-Cu



**Fig. 2 | Structural and compositional analyses of the Ag-Ru-Cu catalysts.** **a–c**, Bright-field scanning transmission electron microscopy image (**a**) and high-angle annular dark-field scanning transmission electron microscopy image (**b**) of the Ag-Ru-Cu catalyst and the corresponding EDX spectroscopy elemental mapping of Cu, Ag and Ru (**c**). Both SEM and TEM measurements were repeated at least twice independently, and similar results were obtained. **d–f**, High-resolution XPS spectra of Cu 2p (**d**), Ag 3d (**e**) and Ru 3p<sub>3/2</sub> (**f**) for the Ag-Ru-Cu catalysts.

electrodes is  $153 \pm 12 \text{ mA cm}^{-2}$ , representing 1.3 times and 1.5 times improvement relative to the Ag-Cu and Cu electrodes, respectively (Fig. 3c).

To evaluate the selectivity towards *n*-propanol versus C<sub>2</sub> products in CORR, we compare the ratios of *n*-propanol FE to total C<sub>2</sub> FE ( $\frac{\text{FE}_{n\text{-PrOH}}}{\text{FE}_{\text{C}_2}}$ ) on different electrodes. Relative to the Ag-Cu and Cu electrodes, the Ag-Ru-Cu electrodes display higher  $\frac{\text{FE}_{n\text{-PrOH}}}{\text{FE}_{\text{C}_2}}$  (Fig. 3d), further suggesting that the co-doping of Ag and Ru in Cu promotes the coupling reaction between C<sub>1</sub> and the C<sub>2</sub> intermediates.

As controls, we also prepared Ag-Au-Cu and Ag-Pd-Cu electrodes (Supplementary Figs. 20–23) and measured their CORR performance (Supplementary Figs. 24 and 25). By comparing the *n*-propanol FEs under the same current densities among different electrodes, we find that Ag-Au-Cu and Ag-Pd-Cu electrodes exhibit lower *n*-propanol selectivity than Ag-Ru-Cu electrodes but higher *n*-propanol selectivity relative to Ag-Cu and Cu electrodes, in agreement with calculations.

We evaluated the CORR stability on the Ag-Ru-Cu electrode at  $300 \text{ mA cm}^{-2}$  in the MEA electrolyser (Fig. 3e and Supplementary Fig. 26). The system maintained a stable full-cell potential of  $-2.64 \pm 0.07 \text{ V}$  during the CORR measurement. Throughout 100 h of continuous operation, an *n*-propanol FE above 32% was maintained using the Ag-Ru-Cu electrode. Transmission electron microscopy (TEM), EDX and XPS analyses on post-reaction catalysts reveal that the Ag-Ru-Cu catalyst retains its structure following extended operation (Supplementary Figs. 27 and 28).

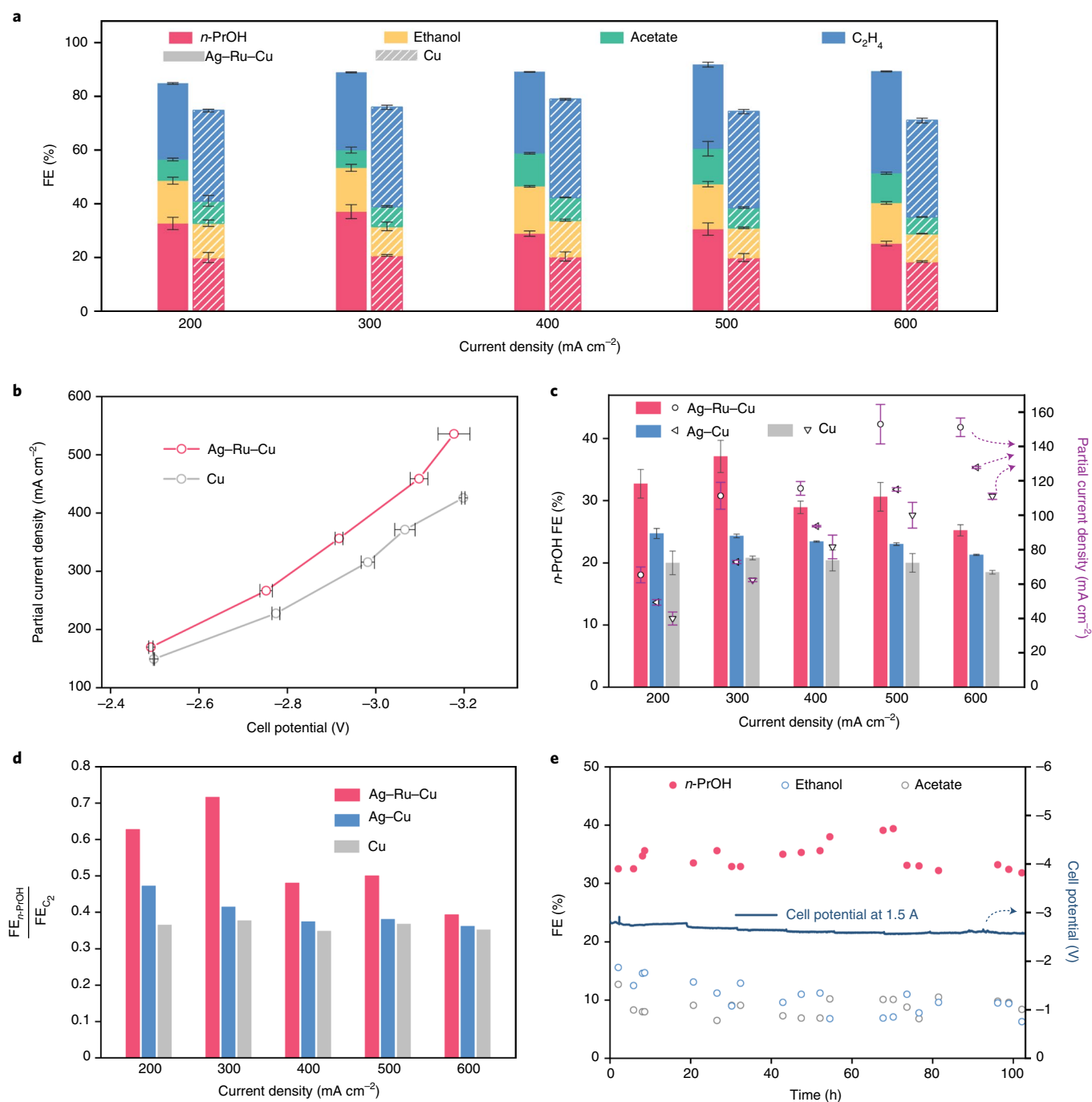
To investigate the chemical state of Cu in different catalysts during CORR, we carried out in situ X-ray absorption spectroscopy (XAS) studies at the Cu K-edge. The Cu K-edge X-ray absorption near-edge structure spectra reveal that under a current density of  $300 \text{ mA cm}^{-2}$ , the average valence states of Cu in Ag-Ru-Cu, Ag-Cu

and Cu are all zero during CORR (Supplementary Fig. 29). We conclude that product selectivities on Ag-Ru-Cu, Ag-Cu and Cu catalysts in CORR are all derived from metallic Cu (refs. <sup>15,32–34</sup>).

To gain insights into the C-C coupling mechanism in different catalysts, we also performed in situ Raman spectroscopy measurements during CORR under different potentials (Fig. 4a and Supplementary Fig. 30). The bands in the range of  $1,900\text{--}2,150 \text{ cm}^{-1}$  arise from the C≡O stretching of the adsorbed CO on metal sites<sup>35–37</sup>, wherein the regions below and above  $2,000 \text{ cm}^{-1}$  are attributed to the bridge-bound CO (CO<sub>bridge</sub>)—which is not an on-pathway intermediate in CORR—and the atop-bound CO (CO<sub>atop</sub>), respectively<sup>35–37</sup>. Relative to Cu, the C≡O stretching bands on Ag-Ru-Cu and Ag-Cu are only from CO<sub>atop</sub> on the surface, indicating that the adsorbed CO on Ag-Ru-Cu and Ag-Cu is in a more favourable configuration for further reaction to C<sub>2+</sub> products compared with Cu (ref. <sup>37</sup>).

In the Raman spectra, the bands located at  $\sim 283 \text{ cm}^{-1}$  and  $\sim 363 \text{ cm}^{-1}$  are associated with frustrated rotation of \*CO on Cu and Cu-CO stretching, respectively. Under the same applied potentials, we observe a blueshift of the Cu-CO stretching band on Ag-Ru-Cu relative to Ag-Cu and Cu (Fig. 4a). The blueshift of the Cu-CO stretching band indicates a stronger Cu-CO bond on the Ag-Ru-Cu surface compared with the Ag-Cu and Cu surfaces<sup>38</sup>, which might favour the C-C coupling step and subsequent generation of C<sub>2+</sub> products<sup>5,39</sup>. As controls, we also acquired in situ Raman spectra with the Ar-saturated KOH electrolyte to confirm that the peaks in the regions marked orange, blue and yellow arise from the conditions of CORR (Fig. 4a and Supplementary Fig. 31).

We investigated the extent to which *n*-propanol electrosynthesis can be scaled, seeking to increase the active area to  $15 \text{ cm}^2$  ( $A = 15 \text{ cm}^2$ ; Fig. 4b, Supplementary Figs. 32 and 33 and Supplementary Table 6). We achieved, at a current density of  $300 \text{ mA cm}^{-2}$ ,



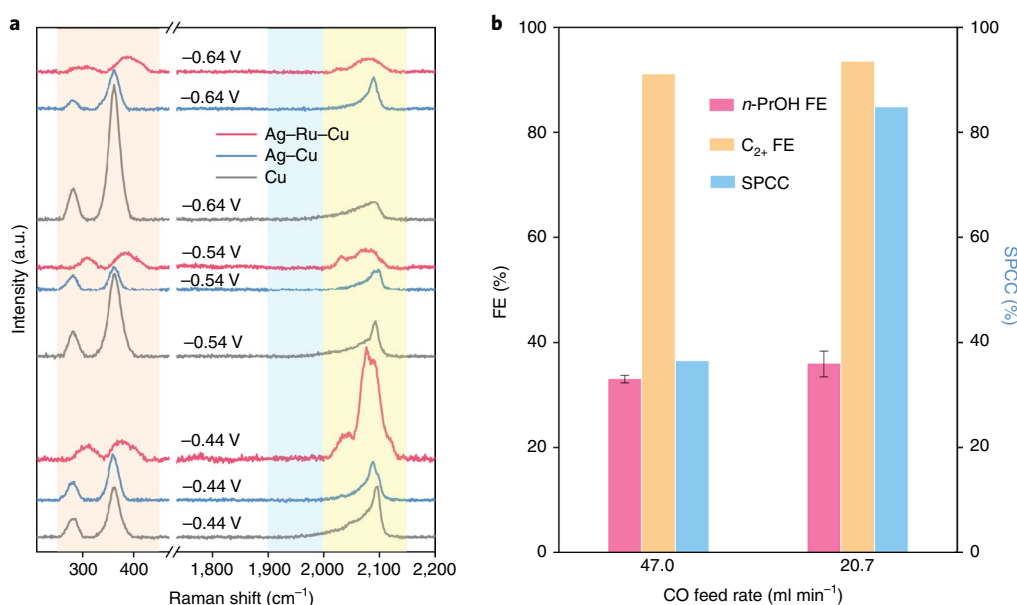
**Fig. 3 | CORR performance of different cathode electrodes.** **a**,  $C_{2+}$  product distribution under different current densities for Ag-Ru-Cu and Cu electrodes. Error bars represent the standard deviation of three independent samples. Data are presented as mean values  $\pm$  standard deviation. **b**, Partial current densities of  $C_{2+}$  products for Ag-Ru-Cu and Cu electrodes under different potentials. Error bars represent the standard deviation of potentials ( $>660$  data points collected in one experiment) during the constant current electrolysis. Data are presented as mean values  $\pm$  standard deviation. **c**, *n*-Propanol (*n*-PrOH) FEs and partial *n*-propanol current densities on different electrodes at various current densities. Error bars represent the standard deviation of three independent samples. Data are presented as mean values  $\pm$  standard deviation. **d**, Comparison of  $\frac{FE_{n-PrOH}}{FE_{C_{2+}}}$  ratios on different electrodes at various current densities. **e**, Liquid product distribution and cell voltage during 102 h operation of CORR at a constant current of 1.5 A. CO feed rate in all these experiments is  $47.0 \text{ ml min}^{-1}$ .

*n*-propanol FE of  $36\% \pm 3\%$  and a  $C_{2+}$  FE of 93% at a full-cell potential of  $-2.60 \pm 0.02 \text{ V}$  (again, without ohmic loss correction); this corresponds to a full-cell energy efficiency of 37% for all  $C_{2+}$  products. To reduce the energy penalty of unreacted CO and gas product separation after reaction, we pursued a high single-pass CO conversion (SPCC) in the system. We lowered the CO feed rate

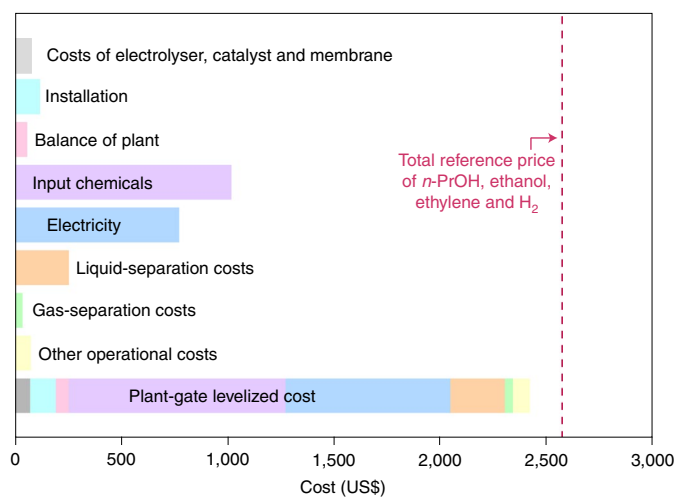
and observed that Ag-Ru-Cu catalysts could retain similar product selectivities at a low CO feed rate; as a result, we achieved a SPCC as high as 85% for  $C_{2+}$  products.

To assess the economic potential of the *n*-propanol electrosynthesis powered by renewable electricity, we performed a TEA for the process, where *n*-propanol, ethanol, ethylene and  $H_2$  products





**Fig. 4 | In situ characterization and *n*-propanol electrosynthesis in a larger electrolyser.** **a**, In situ Raman spectra of different catalysts under different applied potentials versus RHE using 1 M KOH electrolyte during CORR. The regions of 250–450 cm<sup>-1</sup>, 1,900–2,000 cm<sup>-1</sup> and 2,000–2,150 cm<sup>-1</sup> are marked by orange, blue and yellow, respectively. The Raman shift in the range of 470 cm<sup>-1</sup> to 1,735 cm<sup>-1</sup> is marked by the break in the x axis. **b**, FEs towards *n*-propanol and C<sub>2+</sub> products and SPCC with different CO feed rates at the applied current of 4.5 A in the A = 15 cm<sup>2</sup> MEA electrolyser. Error bars represent the standard deviation of three independent samples. Data are presented as mean values ± standard deviation.



**Fig. 5 | Breakdown of the plant-gate levelized cost per tonne of *n*-propanol and the corresponding quantity of ethanol, ethylene and H<sub>2</sub> produced on Ag-Ru-Cu at a current density of 300 mA cm<sup>-2</sup>.** The TEA findings are calculated based on the CORR performance in the A = 15 cm<sup>2</sup> MEA electrolyser with a CO feed rate of 20.7 ml min<sup>-1</sup>. The total reference price of *n*-propanol, ethanol and H<sub>2</sub> is marked by the red dashed line.

are considered as the products for sale in the calculation (Fig. 5, Supplementary Figs. 34 and 35 and Supplementary Table 7). We accounted for the cost of separation, including the separation of liquid products from one another and gas products from one another; the costs for the electrolyser, catalyst, membrane, installation, balance of plant, input chemicals and electricity; and the other operational costs (such as labour and maintenance; Supplementary Methods). Sensitivity analysis reveals that the plant-gate levelized cost depends most importantly on electricity cost and on electrochemical performance parameters such as *n*-propanol FE, current

density, SPCC and full-cell potential (Supplementary Fig. 35, and Supplementary Table 7). Further calculation reveals that with an *n*-propanol FE of 36%, the renewable electricity-powered *n*-propanol electrosynthesis becomes profitable only when the current density is higher than 150 mA cm<sup>-2</sup> and SPCC is above 15% (Supplementary Fig. 36).

The TEA calculation—based on the CORR performance data at 300 mA cm<sup>-2</sup> in the A = 15 cm<sup>2</sup> MEA electrolyser—shows that the plant-gate levelized cost for 1 tonne of *n*-propanol, plus the corresponding quantity of ethanol, ethylene and H<sub>2</sub> produced at 300 mA cm<sup>-2</sup> on Ag-Ru-Cu electrodes, is projected to be less than the sum of their reference prices (Fig. 5). This result suggests that the CORR on the Ag-Ru-Cu electrodes under the above conditions shows promise.

## Conclusions

We report Ag-Ru-Cu catalysts that enable *n*-propanol FE of 37% ± 3% at a partial current density of 111 ± 9 mA cm<sup>-2</sup> during CORR. We also achieve 100 h stable *n*-propanol electrosynthesis at 300 mA cm<sup>-2</sup>. The performance of Ag-Ru-Cu electrodes outperforms other reported *n*-propanol electrosynthesis in selectivity, current density and operation time. We scale *n*-propanol electrosynthesis to 15 cm<sup>2</sup> MEA, achieving the performance, including *n*-propanol FE of 36% ± 3% and a C<sub>2+</sub> FE of 93% at the full-cell potential of -2.60 ± 0.02 V, together with an SPCC of 85% and full-cell energy efficiency of 37% for all C<sub>2+</sub> products. The TEA suggests the CORR-to-*n*-propanol system has a path to become profitable. This work paves a way for the efficient electrosynthesis of C<sub>3</sub> products and the decarbonization of the petrochemical industry.

## Methods

**Chemicals.** Silver nitrate (AgNO<sub>3</sub>, 99.0%), ruthenium (III) chloride hydrate (RuCl<sub>3</sub>·xH<sub>2</sub>O) and iridium (III) chloride hydrate (IrCl<sub>3</sub>·xH<sub>2</sub>O, 99.9%) were purchased from Sigma-Aldrich. Potassium hydroxide (KOH) was received from Caledon Laboratory Chemical. Anion-exchange membrane (Fumasep FAA-3-50) and titanium mesh were received from Fuel Cell Store. Sustainion anion-exchange membrane was purchased from Dioxide Materials. The anion-exchange membranes were activated before use<sup>5</sup>. Copper target (99.999%) was purchased from Kurt J. Lesker.

Polytetrafluoroethylene membrane with an average pore size of 450 nm was received from Beijing Zhongxingweiyi Instrument. All chemicals were used as received. The aqueous solutions were prepared using distilled water with a resistivity of 18.2 MΩ cm.

**Preparation of electrodes.** We first prepared a conductive gas-diffusion layer by sputtering 50-nm-thick Cu (Cu target, sputtering rate  $\sim 0.6 \text{ \AA s}^{-1}$ ) on a piece of PTFE membrane using a magnetron sputtering system. Cu nanoparticles (Sigma-Aldrich) were dispersed in a mixture of methanol and Nafion perfluorinated resin solution (5 wt% in a mixture of lower aliphatic alcohols and water; Sigma-Aldrich) under ultrasonication for 30 min to prepare a suspension with a Cu concentration of  $9.9 \text{ mg ml}^{-1}$ . The suspension was spray coated on the gas-diffusion layer with a Cu nanoparticle loading of  $6 \text{ mg cm}^{-2}$  to prepare the Cu electrode. For the experiments in the  $A = 15 \text{ cm}^2$  MEA electrolyser, the Cu electrode was prepared by directly spray coating the suspension on the carbon-based gas-diffusion layer.

To prepare the Ag–Ru–Cu electrode, we first immersed the prepared Cu electrode in a  $\text{N}_2$ -saturated  $5 \mu\text{mol l}^{-1}$   $\text{RuCl}_3$  aqueous solution at  $65^\circ\text{C}$  for 20 min and then immersed the electrode in a  $\text{N}_2$ -saturated  $5 \mu\text{mol l}^{-1}$   $\text{AgNO}_3$  aqueous solution at  $65^\circ\text{C}$  for 2 h. The Ag–Cu electrode, Ag–Au–Cu electrode and Ag–Pd–Cu electrode were prepared using a similar galvanic-replacement approach. For the Ag–Cu electrode, the prepared Cu electrode was immersed in  $\text{N}_2$ -saturated distilled water at  $65^\circ\text{C}$  for 20 min and then in a  $\text{N}_2$ -saturated  $5 \mu\text{mol l}^{-1}$   $\text{AgNO}_3$  aqueous solution at  $65^\circ\text{C}$  for 2 h. For the Ag–Au–Cu electrode, the prepared Cu electrode was immersed in a  $\text{N}_2$ -saturated  $5 \mu\text{mol l}^{-1}$   $\text{HAuCl}_4$  aqueous solution at  $40^\circ\text{C}$  for 15 min and then in a  $\text{N}_2$ -saturated  $5 \mu\text{mol l}^{-1}$   $\text{AgNO}_3$  aqueous solution at  $65^\circ\text{C}$  for 2 h. For the Ag–Pd–Cu electrode, the prepared Cu electrode was immersed in a  $\text{N}_2$ -saturated  $5 \mu\text{mol l}^{-1}$   $\text{H}_2\text{PdCl}_4$  aqueous solution at  $65^\circ\text{C}$  for 20 min and then in a  $\text{N}_2$ -saturated  $5 \mu\text{mol l}^{-1}$   $\text{AgNO}_3$  aqueous solution at  $65^\circ\text{C}$  for 2 h. The anode catalyst is titanium mesh-supported iridium oxide ( $\text{IrO}_2/\text{Ti}$  mesh) prepared by a previously reported dip coating and thermal decomposition method<sup>40</sup>.

**Materials characterization.** SEM images were taken using a Hitachi FE-SEM SU5000 microscope. High-angle annular dark-field scanning transmission electron microscopy images and the corresponding EDX elemental mapping were taken using a Hitachi HF-3300 microscope at 300 kV. Cathode structure and surface composition characterization were carried out using XRD (MiniFlex600) with Cu-K $\alpha$  radiation and XPS (model 5600, PerkinElmer) with a monochromatic aluminium X-ray source, respectively.

In situ Raman measurements were performed using a Renishaw inVia Raman Microscope (water immersion objective ( $\times 63$ ), 785 nm laser) in a modified flow cell with 1 M KOH aqueous solution as the electrolyte (Supplementary Fig. 30). The different prepared cathode catalysts, Ag/AgCl reference electrode (3 M KCl, BASi) and platinum coil were used as the working electrodes, reference electrode and counter electrode, respectively. CO or Ar was continuously supplied to the gas chamber during the measurement. The potentials ( $E$ ) in Raman measurement were converted to values versus the reversible hydrogen electrode (RHE) using the equation:  $E_{\text{RHE}} = E_{\text{Ag/AgCl}} + 0.210 \text{ V} + 0.0591 \times \text{pH}$ .

In situ XAS measurements were conducted at BL-17C at the National Synchrotron Radiation Research Center. We measured in situ XAS spectra at  $300 \text{ mA cm}^{-2}$  during CORR using a flow-cell reactor, a configuration the same as that used in a previous report<sup>5,23</sup>. In the flow-cell reactor, an Ag/AgCl reference electrode (3 M KCl, BASi; reference electrode), Ni foam (1.6 nm thickness, MTI Corporation; anode) and anion-exchange membrane (Fumasep FAB-PK-130, Fuel Cell Store; membrane) were used. 1 M KOH aqueous solution was used as the electrolyte, and CO (Linde, 99.99%) was continuously supplied to the gas chamber during CORR. XAS data were processed using ATHENA and ARTEMIS software included in a standard IFFFIT package<sup>41</sup>.

**Electrochemical measurements.** Without specification, all the CORR performance was measured in the  $A = 5 \text{ cm}^2$  MEA electrolyser (SKU: 68732; Dioxide Materials) (Supplementary Figs. 14 and 15). The MEA electrolyser installation procedure is the same as that used in our previous report<sup>5</sup>. For the  $A = 15 \text{ cm}^2$  MEA electrolyser (Supplementary Fig. 32), the cathode electrode ( $3.875 \text{ cm} \times 3.875 \text{ cm}$ ) was positioned on the cathode side and thus the activated Sustainion membrane ( $6.5 \text{ cm} \times 6.5 \text{ cm}$ ) and an  $\text{IrO}_2/\text{Ti}$  mesh anode electrode ( $3.875 \text{ cm} \times 3.875 \text{ cm}$ ) was put on top of the cathode, successively; all were assembled in the MEA electrolyser.

The MEA electrolyser-based CORR measurement procedure is similar to that used in a previous report<sup>5</sup>. CO gas (Linde, 99.99%) at different feed rates flowed to the humidifier with distilled water continuously and was then supplied to the cathode chamber. Anolyte (1 M KOH aqueous solution) was introduced into the anode chamber and was circulated using a pump ( $10 \text{ ml min}^{-1}$ ). Using an electrochemical station (AUT50783) equipped with a current booster (10 A), we evaluated the performance of the cathode electrode in a two-electrode system at different current densities. The long-term operation test was also performed in the MEA electrolyser, and the anion-exchange membrane (Fumasep FAB-PK-130) was used as the membrane. The products from the cathode side went through a simplified cold trap that was used for separating liquid products and gas products. The gas products were tested by gas chromatograph (PerkinElmer Clarus 600). The

liquid products were analysed using a NMR spectrometer (Agilent DD2 600 MHz) with dimethylsulfoxide as an internal standard. Liquid product FE was calculated by considering the total amount of the products collected from anode and cathode sides in the same period.

**Full-cell energy efficiency calculation.** For different products, A (*n*-propanol, ethanol, ethylene and acetate), the full-cell energy efficiency for product A is calculated as follows<sup>5</sup>:

$$EE_{\text{full cell, A}} = \frac{(1.23 + (-E_A^0)) \times FE_A}{-E_{\text{full cell}}}$$

where  $E_A^0$  is the thermodynamic potential of CO to product A ( $E_{\text{n-PrOH}}^0 = 0.20 \text{ V}$  versus RHE;  $E_{\text{ethanol}}^0 = 0.178 \text{ V}$  versus RHE;  $E_{\text{ethylene}}^0 = 0.17 \text{ V}$  versus RHE;  $E_{\text{acetate}}^0 = 0.454 \text{ V}$  versus RHE) calculated based on the standard molar Gibbs energy formation at 298.15 K (refs. 23,42).  $FE_A$  is the measured FE (%) of the product A, and  $E_{\text{full-cell}}$  is the full-cell voltage measured in the MEA system without ohmic loss correction.

**SPCC calculation.** Under the conditions of 298.15 K and 101.3 kPa, SPCC is calculated as follows:

$$\text{Total SPCC} = 60 \text{ (s)} \times \frac{\text{Total current (A)} \times FE_A \times \text{Molar ratio} \left( \frac{\text{CO}}{\text{product A}} \right)}{\text{Electrons transferred for every product A molecule} \times \text{Faraday's constant}} \\ \div \frac{\text{CO feed rate} \left( \frac{\text{L}}{\text{min}} \right) \times 1 \text{ (min)}}{8.314 \left( \text{J mol}^{-1} \text{ K}^{-1} \right) \times 298.15 \text{ (K)}} \times \frac{101,300 \text{ (Pa)}}{1}$$

**DFT calculations.** All ab initio DFT calculations were performed by employing the projector-augmented wave method as implemented in the Vienna Ab initio Simulation Package<sup>43–46</sup>. The generalized gradient approximation in the parametrization of Perdew–Burke–Ernzerhof was implemented to describe the exchange–correlation functional<sup>47</sup>. A plane-wave cut-off of 450 eV and  $2 \times 4 \times 1$  gamma-centred  $k$ -point grids generated by the Monkhorst–Pack scheme were used for all the calculations<sup>48</sup>. A vacuum region of more than  $15 \text{ \AA}$  thickness was included along the perpendicular direction to avoid artificial interactions. The zero damping DFT–D3 method of Grimme was employed to better capture long-range dispersion interactions<sup>49</sup>.

The Ag–Cu (111) and Cu (111) structures were constructed based on our previous study<sup>23</sup>. For the screened Ag–X–Cu (X: Au, Pd, Pt, Ni, Fe and Ru) systems, one Cu atom on the top layer of a four layer ( $6 \times 3$ ) Ag–Cu (111) supercell was substituted with Au, Pd, Pt, Ni, Fe and Ru (Supplementary Figs. 1–8). The position of the substituted atom was determined by the structure with the lowest energy in our benchmark calculations (Supplementary Note 1 and Supplementary Fig. 9). The number of adsorbed \*CO near the coupling sites was determined using the adsorption energy of \*CO on Ag–X–Cu relative to Cu (Supplementary Note 1 and Supplementary Table 2). A monolayer of charged water molecules was included in all initial, transition and final states of  $C_1$ – $C_1$  and  $C_1$ – $C_2$  coupling above the surface to account for the combined field and solvation effects<sup>50</sup>. Geometries of the initial and final states were optimized by a force-based conjugate gradient algorithm with two upper layers together with the water molecules and adsorbates being allowed to relax, while the atoms in the two lower layers were fixed. The transition states were located using the climbing image nudged elastic band method<sup>51</sup>. The Gibbs free energy ( $\Delta G$ ) for  $C_1$ – $C_1$  and  $C_1$ – $C_2$  coupling was calculated by converting the electronic energy using the equation:  $\Delta G = \Delta E + \Delta ZPE + \int \Delta C_p dT - T \Delta S$ , where  $\Delta E$ ,  $\Delta ZPE$ ,  $\Delta C_p$ , and  $\Delta S$  are the differences in electronic energy, zero-point energy, heat capacity and entropy, respectively, and  $T$  is set to room temperature (298.15 K). Here DFT calculations do not explicitly consider the dynamic changes in the surface richness of Ag–Ru–Cu. The theoretical exploration of dynamic changes of the surface under catalysis will be an important aspect of future studies.

## Data availability

All data are available within the paper, Supplementary Information and source data files. Source data are provided with this paper.

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## Author contributions

E.H.S. supervised the project. X.W. and E.H.S. conceived the idea. X.W. designed and carried out the experiments. P.O. carried out DFT calculations. S.-F.H. performed XAS measurements. S.-F.H. and J.A. analysed the XAS data. A.O. fabricated the IrO<sub>x</sub>-coated Ti mesh electrodes. J.T. and J.Y.H. contributed to the SEM and TEM characterization. X.W. and J.S. did the TEA. K.B. and ASR carried out XPS measurements. X.W. and M.S. performed XRD measurements. C.M.G. and F.P.G.d.A. contributed to the manuscript editing. X.W., P.O., and E.H.S. co-wrote the manuscript. R.K.M., C.P.O., Z.W., A.H.I. and D.S. assisted with the discussions. All authors discussed the results and assisted during manuscript preparation.

## Competing interests

X.W. and E.H.S. have filed a provisional patent application titled 'Manufacturing and use of co-doped multi-metallic electrocatalysts for upgrading of CO to propanol' (application number 63/192,842). All other authors declare no competing interests.

## Additional information

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